



*MEC516/BME516:  
Fluid Mechanics I*

*Chapter 4: Differential Relations for  
Fluid Flow  
Part 4*

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RYERSON  
UNIVERSITY

Department of Mechanical  
& Industrial Engineering

# Overview

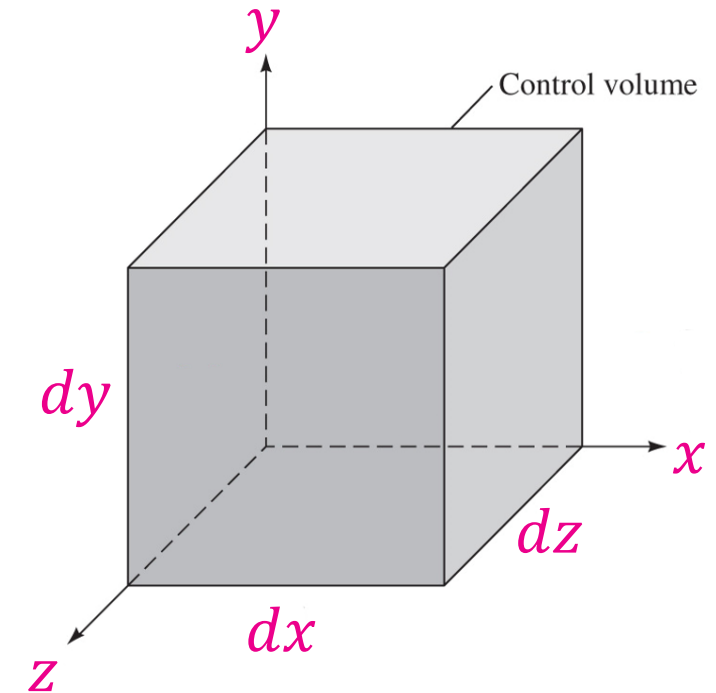
- **Differential form of conservation of linear momentum for fluids**

- Examine the forces on a differential fluid element
- $F = ma$  for a differential fluid element
- Navier-Stokes Equations (for a Newtonian fluid)

(This is an overview -- a detailed derivation is beyond the scope of this course)

- **Example**

Determine if a given velocity vector field  $\mathbf{V}(x, y, z, t)$  satisfies conservation of momentum.



# Conservation of Linear Momentum

- Consider a differential fluid control volume. The elemental volume has mass  $dm = \rho dV = \rho dx dy dz$

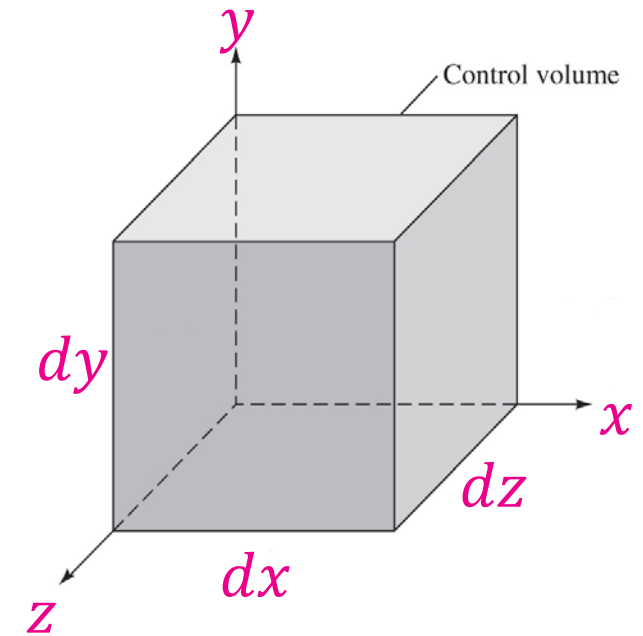
- Now we apply Newton's second law to this differential mass:

$$\sum \mathbf{F} = dm \mathbf{a} = (\rho dx dy dz) \mathbf{a}$$

- We showed that the total fluid acceleration is:

$$\mathbf{a} = \frac{d\mathbf{V}}{dt} = \frac{D\mathbf{V}}{Dt} = \frac{\partial \mathbf{V}}{\partial t} + \left( u \frac{\partial \mathbf{V}}{\partial x} + v \frac{\partial \mathbf{V}}{\partial y} + w \frac{\partial \mathbf{V}}{\partial z} \right)$$

- So, we get:  $\sum \mathbf{F} = \rho \frac{d\mathbf{V}}{dt} dx dy dz = \rho \left\{ \frac{\partial \mathbf{V}}{\partial t} + \left( u \frac{\partial \mathbf{V}}{\partial x} + v \frac{\partial \mathbf{V}}{\partial y} + w \frac{\partial \mathbf{V}}{\partial z} \right) \right\} dx dy dz$  Eq. (1)



# Forces on the Differential Fluid Element

- There are two types of forces on the differential fluid element:
  - (i) Body Forces
  - (ii) Surface Forces

## (i) Body Forces

- Body forces are uniformly distributed through the element.
- For the purpose of this course, the only body force we will consider is gravity. (Others are possible, e.g. magnetic forces, MHD)

- Define the gravity vector:

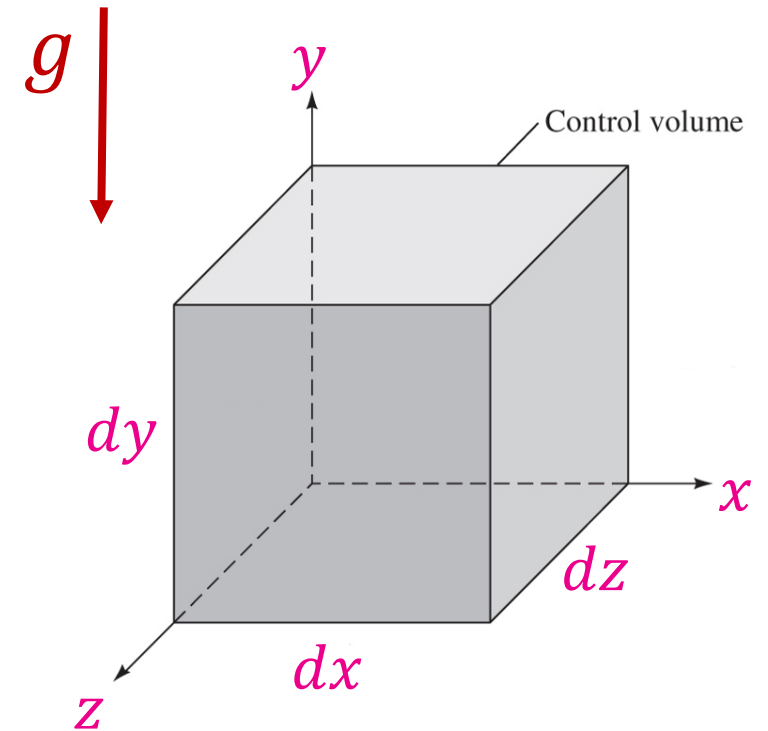
The gravity force on the element is

Often, the y-axis is upward, then:

$$\mathbf{g} = g_x \mathbf{i} + g_y \mathbf{j} + g_z \mathbf{k}$$

$$d\mathbf{F}_{grav} = \rho \mathbf{g} dx dy dz$$

$$g_x = 0, g_y = -g, g_z = 0$$



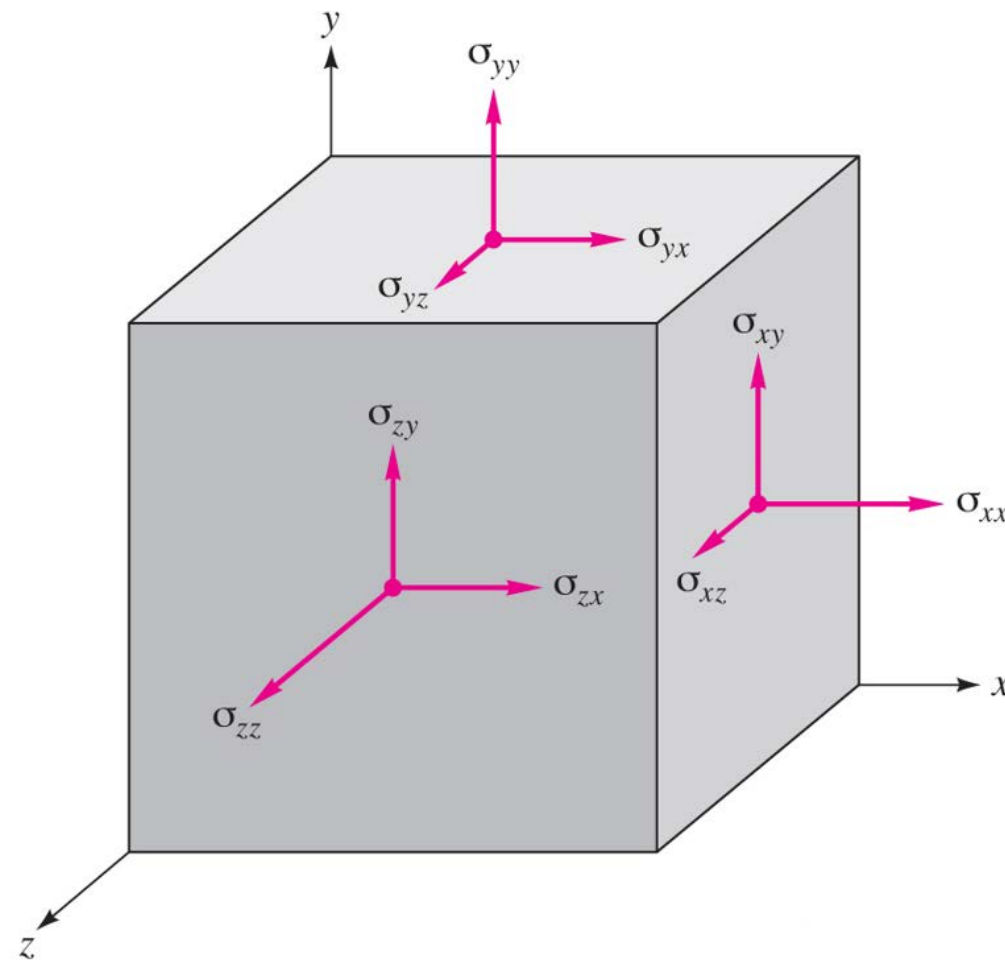
# Forces on the Differential Fluid Element

## (ii) Surface Forces

- The surface forces per unit area (stresses) on the fluid are due to:
  - viscous stress ( $\tau$ )
  - pressure ( $p$ )
- This gives rise to nine components of stress:

$$\sigma_{ij} = \begin{vmatrix} -p + \tau_{xx} & \tau_{yx} & \tau_{zx} \\ \tau_{xy} & -p + \tau_{yy} & \tau_{zy} \\ \tau_{xz} & \tau_{yz} & -p + \tau_{zz} \end{vmatrix} \begin{matrix} \leftarrow \text{x-direction} \\ \leftarrow \text{y-direction} \\ \leftarrow \text{z-direction} \end{matrix}$$

$\sigma_{ij}$  = Stress in  $j$   
direction on a face  
normal to  $i$  axis



# Forces on the Differential Fluid Element

- The net surface forces in the x-direction:

$$dF_x = \frac{\partial \sigma_{xx}}{\partial x} dx(dydz) + \frac{\partial \sigma_{yx}}{\partial y} dy(dx dz) + \frac{\partial \sigma_{zx}}{\partial z} dz(dx dy)$$

$$dF_x = \left\{ \frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{yx}}{\partial y} + \frac{\partial \sigma_{zx}}{\partial z} \right\} dx dy dz$$

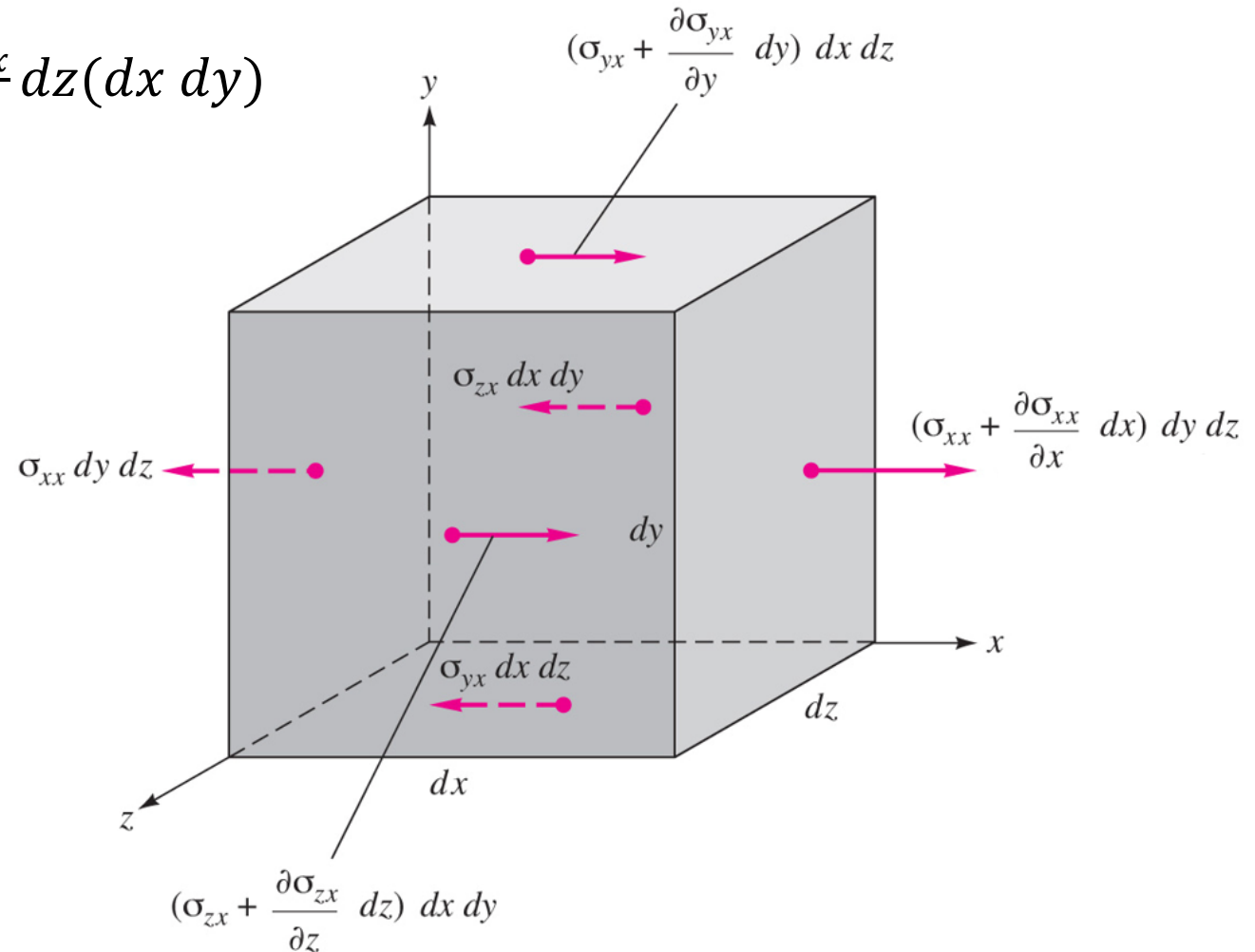
Similarly,

- The net surface forces in the y-direction:

$$dF_y = \left\{ \frac{\partial \sigma_{xy}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \sigma_{zy}}{\partial z} \right\} dx dy dz$$

- The net surface forces in the z-direction:

$$dF_z = \left\{ \frac{\partial \sigma_{xz}}{\partial x} + \frac{\partial \sigma_{yz}}{\partial y} + \frac{\partial \sigma_{zz}}{\partial z} \right\} dx dy dz$$



# Forces on the Differential Fluid Element

- For a Newtonian fluid, it can be shown that the viscous stresses are related to the velocity field as follows:

$$\begin{aligned}\tau_{xx} &= 2\mu \frac{\partial u}{\partial x} & \tau_{yy} &= 2\mu \frac{\partial v}{\partial y} & \tau_{zz} &= 2\mu \frac{\partial w}{\partial z} \\ \tau_{xy} = \tau_{yx} &= \mu \left( \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) & \tau_{xz} = \tau_{zx} &= \mu \left( \frac{\partial w}{\partial x} + \frac{\partial u}{\partial z} \right) \\ \tau_{yz} = \tau_{zy} &= \mu \left( \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right)\end{aligned}$$

These are the “drag” forces on the fluid caused by fluid viscosity, i.e. fluid friction.

- Now we apply Newton’s second law, Eq. (1):

$$\sum \mathbf{F} = \rho \frac{dV}{dt} dx dy dz = \rho \left\{ \frac{\partial V}{\partial t} + \left( u \frac{\partial V}{\partial x} + v \frac{\partial V}{\partial y} + w \frac{\partial V}{\partial z} \right) \right\} dx dy dz \quad \text{Eq. (1)}$$

As discussed, the sum of the forces  $\sum \mathbf{F}$  include: (i) pressure forces, (ii) viscous forces, and (iii) gravity force.

# The Navier-Stokes Equations

For a Newtonian fluid with constant properties ( $\rho = \text{const}$ ,  $\mu = \text{const}$ ):

x-momentum:

$$\rho \left( \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) = - \frac{\partial p}{\partial x} + \mu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) + \rho g_x$$

y-momentum:

$$\rho \left( \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} \right) = - \frac{\partial p}{\partial y} + \mu \left( \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} \right) + \rho g_y$$

z-momentum:

$$\rho \left( \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} \right) = - \frac{\partial p}{\partial z} + \mu \left( \frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2} \right) + \rho g_z$$



# The Navier-Stokes Equations

These equation represents conservation of momentum in the 3 coordinate directions. They are  $\mathbf{F}=\mathbf{ma}$  on a per unit volume basis.

Let's look at the terms in the x-equation, and the units:

$$\rho \left( \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) = - \frac{\partial p}{\partial x} + \mu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) + \rho g_x$$

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mass per
acceleration
pressure force
viscous force
gravity force per

unit volume
(local and convective)
per unit vol.
per unit vol.
unit vol.

$$\frac{kg}{m^3} \quad \frac{m}{s^2} \quad = \quad \frac{N}{m^3} \quad \frac{N}{m^3} \quad \frac{N}{m^3}$$

# Navier-Stokes Equations

- The constant property Navier-Stokes equations can be written in a compact form using vector notation:

$$\rho \left( \frac{\partial \mathbf{V}}{\partial t} + \mathbf{V} \cdot \nabla \mathbf{V} \right) = -\nabla p + \mu \nabla^2 \mathbf{V} + \rho \mathbf{g}$$

where  $\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$  is the Laplace Operator.

# Cylindrical Coordinates

- As previously discussed, it is sometimes desirable to work in cylindrical coordinates.
- The constant property Navier-Stokes equations are given in Appendix D:

The  $r$ -momentum equation:

$$\frac{\partial v_r}{\partial t} + (\mathbf{V} \cdot \nabla)v_r - \frac{1}{r}v_\theta^2 = -\frac{1}{\rho}\frac{\partial p}{\partial r} + g_r + \nu\left(\nabla^2 v_r - \frac{v_r}{r^2} - \frac{2}{r^2}\frac{\partial v_\theta}{\partial \theta}\right) \quad (\text{D.5})$$

The  $\theta$ -momentum equation:

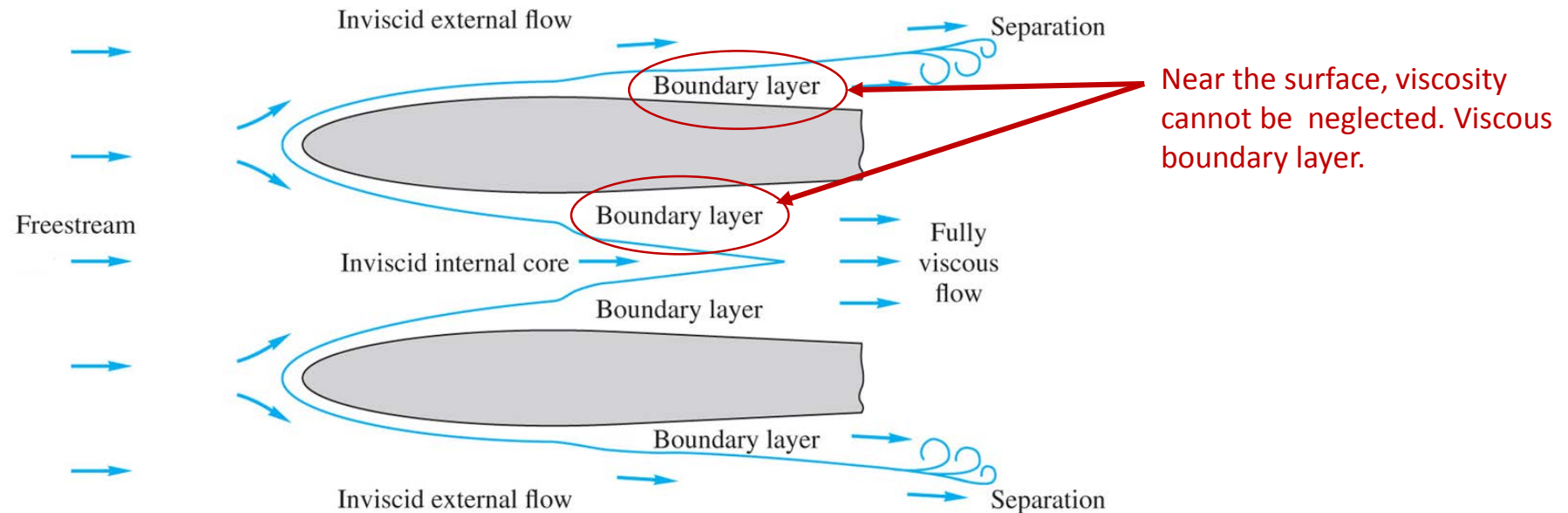
$$\frac{\partial v_\theta}{\partial t} + (\mathbf{V} \cdot \nabla)v_\theta + \frac{1}{r}v_r v_\theta = -\frac{1}{\rho r}\frac{\partial p}{\partial \theta} + g_\theta + \nu\left(\nabla^2 v_\theta - \frac{v_\theta}{r^2} + \frac{2}{r^2}\frac{\partial v_r}{\partial \theta}\right) \quad (\text{D.6})$$

The  $z$ -momentum equation:

$$\frac{\partial v_z}{\partial t} + (\mathbf{V} \cdot \nabla)v_z = -\frac{1}{\rho}\frac{\partial p}{\partial z} + g_z + \nu\nabla^2 v_z \quad (\text{D.7})$$

# Inviscid Flow and Euler's Equation

- Flows with no viscosity are called *Inviscid Flows*. All real fluids have viscosity → idealization.
- Far away from solid surfaces, real flows can be *approximated* as inviscid. Flow fields behaves like  $\mu=0$ .



- For inviscid flows ( $\mu = \tau_{ij} = 0$ ) the Navier-Stokes equations simplify to: 
$$\rho \frac{dV}{dt} = -\nabla p + \rho g$$

This is called *Euler's Equation*.

# Inviscid Flow and Euler's Equation

$$\rho \frac{dV}{dt} = -\nabla p + \rho g$$

*Euler's Equation* can be integrated along a streamline to give the Bernoulli Equation.

## History

- This equation was derived (in 1757) **before** the equations for viscous flow.
- Leonhard Euler, 18<sup>th</sup> century Swiss engineer, physicist and mathematician.
  - Classical beam theory, Euler buckling load
  - Euler formula:  $e^{ix} = \cos(x) + i \sin(x)$



Leonhard Euler, 1707-1783

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## Example

Consider steady incompressible flow of a Newtonian fluid with the velocity field:

$$\mathbf{V} = -2xy \mathbf{i} + (y^2 - x^2) \mathbf{j} + 0 \mathbf{k}$$

Neglect gravitational effects. Does this velocity field satisfy the conservation of momentum i.e., the Navier-Stokes equations?

### Solution

This is a two-dimensional flow. We need to consider the conservation of momentum in the x- and y-directions.

## Example

$$\mathbf{V} = -2xy \mathbf{i} + (y^2 - x^2) \mathbf{j} + 0 \mathbf{k}$$

$$u = -2xy \quad v = y^2 - x^2 \quad w = 0$$

x-momentum:

$$\rho \left( \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) = -\frac{\partial p}{\partial x} + \mu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) + \rho g_x$$

Making the substitutions:

$$\rho(0 + (-2xy)(-2y) + (y^2 - x^2)(-2x) + 0) = -\frac{\partial p}{\partial x} + \mu(0 + 0 + 0) + 0$$

$$\frac{\partial p}{\partial x} = \rho(-4xy^2 + 2xy^2 - 2x^3) = -2\rho(xy^2 + x^3)$$

# Example

$$\text{v-momentum: } \rho \left( \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} \right) = -\frac{\partial p}{\partial y} + \mu \left( \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} \right) + \rho g_y$$

Making the substitutions:

$$\rho(0 + (-2xy)(-2x) + (y^2 - x^2)(2y) + 0) = -\frac{\partial p}{\partial y} + \mu(-2 + 2 + 0) + 0$$

$$\frac{\partial p}{\partial y} = \rho(-4yx^2 - 2y^3 + 2yx^2) = -2\rho(yx^2 + y^3)$$

$$u = -2xy \quad v = y^2 - x^2 \quad w = 0$$

y-momentum:

$$\rho \left( \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} \right) = -\frac{\partial p}{\partial y} + \mu \left( \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} \right) + \rho g_y$$

Making the substitutions:

$$\rho(0 + (-2xy)(-2x) + (y^2 - x^2)(2y) + 0) = -\frac{\partial p}{\partial y} + \mu(-2 + 2 + 0) + 0$$

$$\frac{\partial p}{\partial y} = \rho(-4yx^2 - 2y^3 + 2yx^2) = -2\rho(yx^2 + y^3)$$



## Example

- So far we have shown that:  $\frac{\partial p}{\partial x} = -2\rho(xy^2 + x^3)$  and  $\frac{\partial p}{\partial y} = -2\rho(yx^2 + y^3)$
- The pressure field  $p(x, y)$  is a single function. To determine if the gradients in the x and y directions are compatible, we evaluate the mixed derivative  $\frac{\partial^2 p}{\partial x \partial y}$
- For a single function, these two mixed derivatives must be the equal:

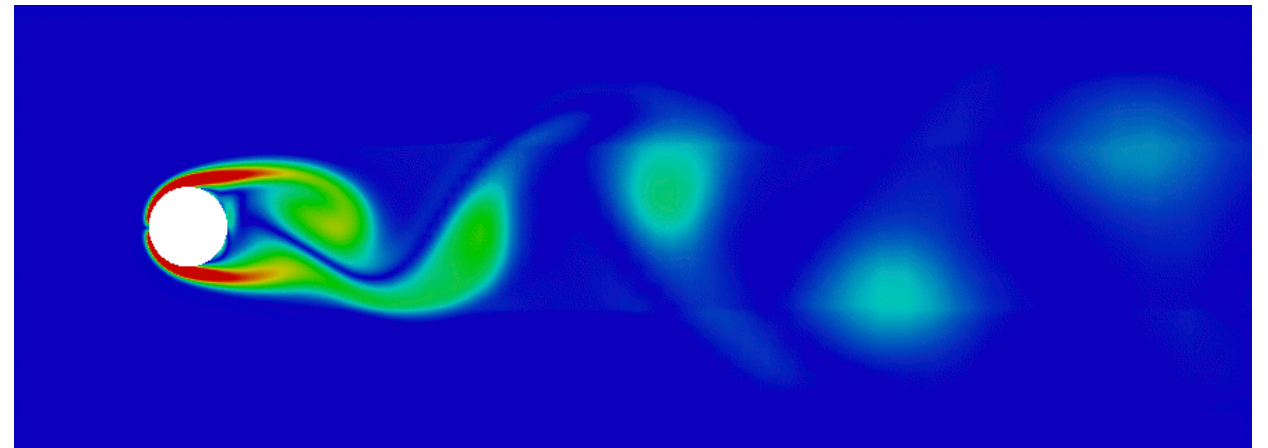
$$\frac{\partial}{\partial y} \left( \frac{\partial p}{\partial x} \right) = \frac{\partial}{\partial y} \left( -2\rho(xy^2 + x^3) \right) = -4\rho xy$$

$$\frac{\partial}{\partial x} \left( \frac{\partial p}{\partial y} \right) = \frac{\partial}{\partial x} \left( -2\rho(yx^2 + y^3) \right) = -4\rho xy$$

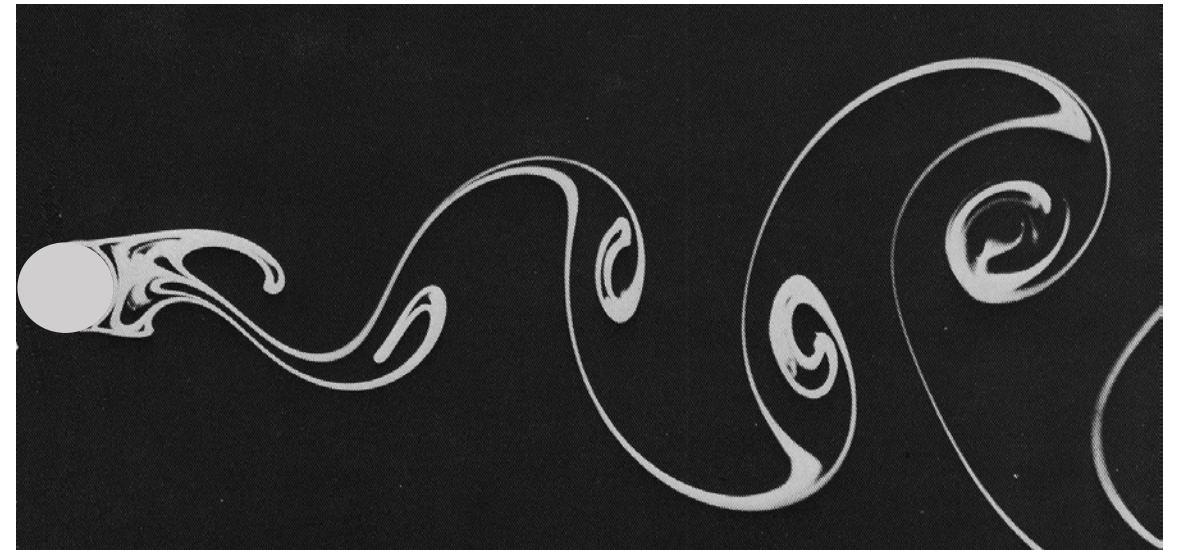
Thus, the velocity field satisfies the Navier-Stokes equations.

Vortex shedding from a cylinder in cross flow  
 $Re \approx 150$ . Solution of the unsteady 2D Navier-Stokes equations.

CFD Prediction



Experimental Flow Visualization



## END NOTES

Presentation prepared and delivered by Dr. David Naylor.

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Sources:

[www.redditian.com](http://www.redditian.com)  
Album of Fluid Motion