



*MEC516/BME516:
Fluid Mechanics I*

*Chapter 4: Differential Relations for
Fluid Flow
Part 3*

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Overview

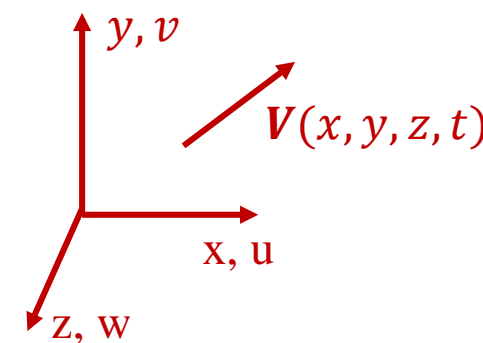
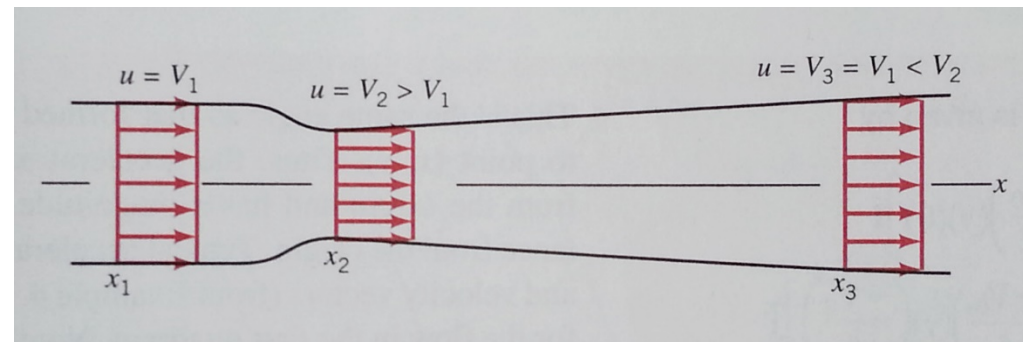
- Derivation of the differential expression for the fluid acceleration field

- “Local” versus “convective” acceleration
- Vector notation

- Examples

- Calculating fluid acceleration in a steady flow in a nozzle (convective acceleration).
- Calculating fluid acceleration field given a velocity vector field, $\mathbf{V}(x, y, z, t)$

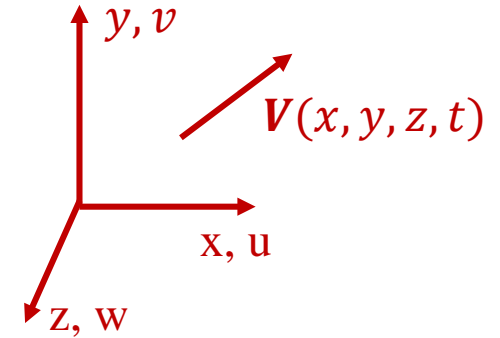
This is vital background for an upcoming discussion of conservation of linear momentum ($\mathbf{F}=\mathbf{m}\mathbf{a}$ for fluids) in differential form i.e., for the *Navier-Stokes* equations.



The Fluid Acceleration Field

- We have been describing fluid flow with a Eulerian velocity vector field:

$$\mathbf{V} = u(x, y, z, t)\mathbf{i} + v(x, y, z, t)\mathbf{j} + w(x, y, z, t)\mathbf{k}$$



- Thus, the acceleration field is:

$$\mathbf{a} = \frac{d\mathbf{V}}{dt} = \frac{du}{dt}\mathbf{i} + \frac{dv}{dt}\mathbf{j} + \frac{dw}{dt}\mathbf{k}$$

- Note that each velocity component is a function of four variables, e.g. $u = u(x, y, z, t)$.
- So, considering only the x-component, to get the total acceleration we must use the chain rule:

$$\frac{du(x, y, z, t)}{dt} = \frac{\partial u}{\partial t} + \frac{\partial u}{\partial x} \frac{\partial x}{\partial t} + \frac{\partial u}{\partial y} \frac{\partial y}{\partial t} + \frac{\partial u}{\partial z} \frac{\partial z}{\partial t}$$

The Fluid Acceleration Field

$$\frac{du(x, y, z, t)}{dt} = \frac{\partial u}{\partial t} + \frac{\partial u}{\partial x} \frac{\partial x}{\partial t} + \frac{\partial u}{\partial y} \frac{\partial y}{\partial t} + \frac{\partial u}{\partial z} \frac{\partial z}{\partial t}$$

- Note that:

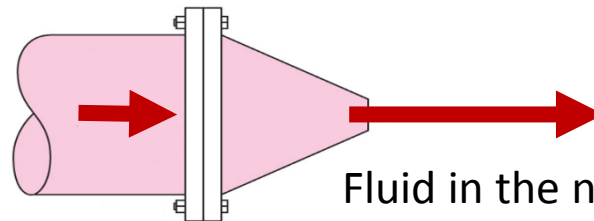
$$\frac{\partial x}{\partial t} = u \quad \frac{\partial y}{\partial t} = v \quad \frac{\partial z}{\partial t} = w$$

convective
acceleration

- Making the substitution, we get:

$$\frac{du(x, y, z, t)}{dt} = \underbrace{\frac{\partial u}{\partial t}}_{\text{local acceleration}} + \underbrace{u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z}}_{\text{convective acceleration}}$$

- Local acceleration* is caused by local unsteady flow e.g., pump speeding up, $Q \uparrow$ in time.
- Convective acceleration* is caused by fluid moving into a region with different velocity. e.g. steady flow through a nozzle.



Fluid in the nozzle accelerates in a steady flow!

The Fluid Acceleration Field

- So the acceleration vector field \mathbf{a} is:

$$\mathbf{a} = \frac{d\mathbf{V}}{dt} = \frac{D\mathbf{V}}{Dt} = \underbrace{\frac{\partial \mathbf{V}}{\partial t}}_{\text{local acceleration}} + \underbrace{\left(u \frac{\partial \mathbf{V}}{\partial x} + v \frac{\partial \mathbf{V}}{\partial y} + w \frac{\partial \mathbf{V}}{\partial z} \right)}_{\text{convective acceleration}}$$

Not an ordinary derivative!

- Most books use the notation $\frac{D\mathbf{V}}{Dt}$ to distinguish this from an ordinary derivative (variable that is a function of only one variable). (The Frank White textbook does not.)
- $\frac{d\mathbf{V}}{dt}$ or $\frac{D\mathbf{V}}{Dt}$ is called the *material derivative* or the *substantial derivative*.

The Fluid Acceleration Field

$$\mathbf{a} = \frac{d\mathbf{V}}{dt} = \frac{D\mathbf{V}}{Dt} = \frac{\partial \mathbf{V}}{\partial t} + \left(u \frac{\partial \mathbf{V}}{\partial x} + v \frac{\partial \mathbf{V}}{\partial y} + w \frac{\partial \mathbf{V}}{\partial z} \right)$$

- The three scalar components can be written as:

x-direction:

$$a_x = \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z}$$

y-direction:

$$a_y = \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z}$$

z-direction:

$$a_z = \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z}$$

The Fluid Acceleration Field

- Vector Notation. This is approaching a “graduate level” discussion...

$$\begin{array}{c}
 \text{\textbf{u i + v j + w k}} \\
 \swarrow \quad \searrow \quad \downarrow \quad \swarrow \quad \searrow \\
 \mathbf{a} = \frac{\partial \mathbf{V}}{\partial t} + \left(u \frac{\partial \mathbf{V}}{\partial x} + v \frac{\partial \mathbf{V}}{\partial y} + w \frac{\partial \mathbf{V}}{\partial z} \right) = \underbrace{\frac{\partial \mathbf{V}}{\partial t} + (\mathbf{V} \cdot \nabla) \mathbf{V}}_{\text{vector notation (compact)}}
 \end{array}$$

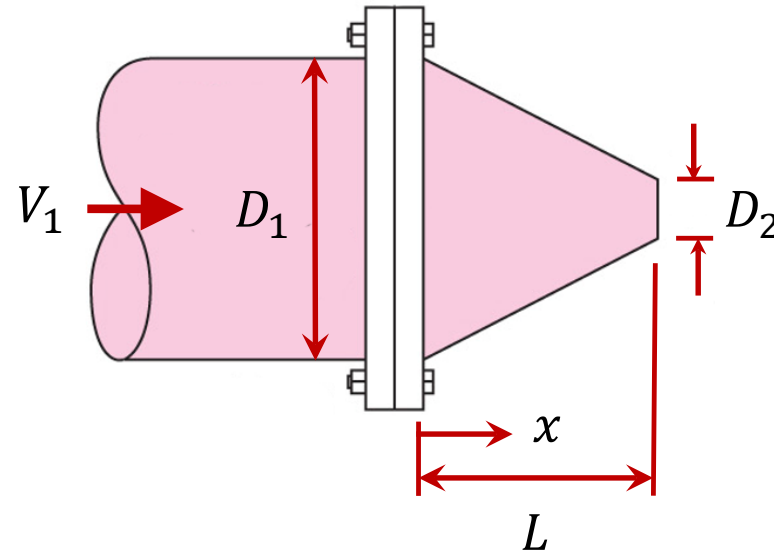
where symbol “ ∇ ” is the *vector gradient* (or *del*) operator: $\nabla = \mathbf{i} \frac{\partial}{\partial x} + \mathbf{j} \frac{\partial}{\partial y} + \mathbf{k} \frac{\partial}{\partial z}$

- So, $\mathbf{V} \cdot \nabla$ becomes an operator: $\mathbf{V} \cdot \nabla = u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} + w \frac{\partial}{\partial z}$

Example 1

Consider a **steady** one-dimensional flow of liquid in nozzle. The incompressible fluid enters the nozzle at velocity V_1 . The nozzle has length L , and inlet diameter D_1 and outlet diameter D_2 .

Derive an analytical expression of the fluid acceleration in the nozzle as a function of the x -coordinate, measured from the nozzle inlet.



Example 1

- Start with general vector expression for fluid acceleration:

$$\mathbf{a} = \frac{\partial \mathbf{V}}{\partial t} + \left(u \frac{\partial \mathbf{V}}{\partial x} + v \frac{\partial \mathbf{V}}{\partial y} + w \frac{\partial \mathbf{V}}{\partial z} \right)$$

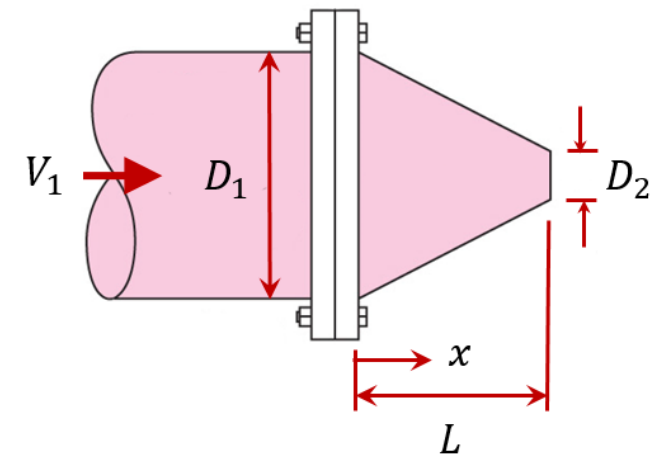
~~0 (steady)~~ ~~0 (1-D)~~ ~~0 (1-D)~~

- Flow is steady. Pump flow rate is not changing. Thus: $\frac{\partial \mathbf{V}}{\partial t} = 0$

- Flow is 1-D: $v = w = 0$ Thus: $\mathbf{V} = u \mathbf{i}$

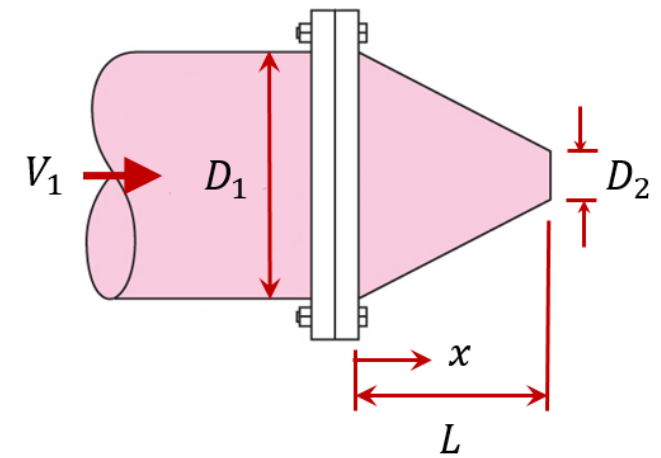
- So, the acceleration equation becomes: $a_x = u \frac{du}{dx}$ (ordinary derivative, $a_x = a_x(x)$ only)

- Next, we need an expression for $u(x)$.



Example 1

$$a_x = u \frac{du}{dx}$$



- Fluid is incompressible: $Q = VA = \text{const} \rightarrow V_1 A_1 = u(x) A(x)$

- From continuity, we note that: $u(x) = \left(\frac{A_1}{A(x)}\right) V_1 = \left(\frac{D_1}{D(x)}\right)^2 V_1$

- The nozzle diameter varies linearly with x : $D(x) = D_1 - \left(\frac{D_1 - D_2}{L}\right) x$

- Making the substitution: $u(x) = \frac{D_1^2 V_1}{\left(D_1 - \left(\frac{D_1 - D_2}{L}\right) x\right)^2}$

- So, the acceleration in x-direction becomes: $a_x = u \frac{du}{dx} = \left[\frac{D_1^2 V_1}{\left(D_1 - \left(\frac{D_1 - D_2}{L}\right) x\right)^2} \right] \frac{-2 D_1^2 \left(-\left(D_1 - D_2\right)/L\right) V_1}{\left(D_1 - \left(\frac{D_1 - D_2}{L}\right) x\right)^3}$

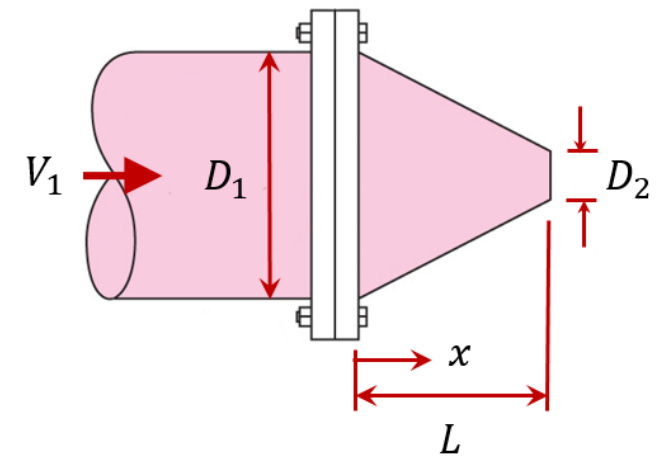
Example 1

- We have the x-acceleration:
$$a_x = \left[\frac{D_1^2 V_1}{\left(D_1 - \left(\frac{D_1 - D_2}{L} \right) x \right)^2} \right] \frac{2 D_1^2 (D_1 - D_2) V_1}{L \left(D_1 - \left(\frac{D_1 - D_2}{L} \right) x \right)^3}$$

- Combining terms:

$$a_x = \frac{2 D_1^4 (D_1 - D_2) V_1^2}{L \left(D_1 - \left(\frac{D_1 - D_2}{L} \right) x \right)^5}$$

- Check units:
$$\frac{m^4 m \frac{m^2}{s^2}}{m m^5} = \frac{m}{s^2}$$



Ans.

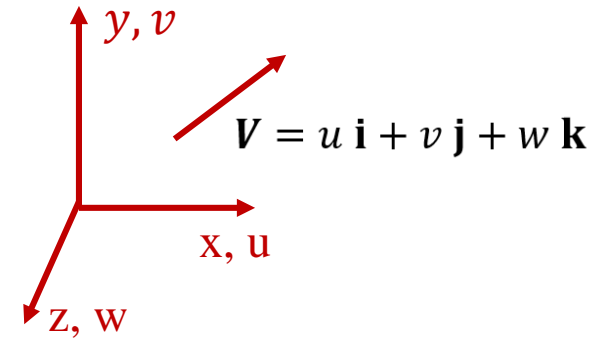
Comments:

- a_x is positive throughout the nozzle. Min. at nozzle inlet, $x = D_1$ & max. at nozzle exit, $x = D_2$.
- This acceleration is purely convective, since the flow is steady. The acceleration occurs because the flow is convected into a region of higher velocity.
- The fluid acceleration produces a thrust on the nozzle in the negative x-direction, $F_x = \dot{m} (V_2 - V_1)$

Example 2

Consider a hypothetical fluid velocity vector field given by:

$$\mathbf{V} = Ct(x^2 - y^2) \mathbf{i} - 2Cxyt \mathbf{j} + 3y \mathbf{k}$$



- (i) Is the flow field steady or unsteady?
- (ii) Obtain an expression for the acceleration vector \mathbf{a} .
- (iii) Evaluate the acceleration vector \mathbf{a} at $(x, y, z, t) = (1, 1, 1, 1)$

Solution

- (i) The flow is unsteady (or transient) since time (t) appears in the velocity vector (which will give rise to local acceleration.)

Example 2

(ii) We have:

$$\mathbf{V} = \overbrace{C t(x^2 - y^2)}^u \mathbf{i} - \overbrace{2Cxyt}^v \mathbf{j} + \overbrace{3y}^w \mathbf{k}$$

- The x-component of acceleration is: $a_x = \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z}$
- Evaluating terms: $a_x = C(x^2 - y^2) + Ct(x^2 - y^2)(2Cxt) + (-2Cxyt)(-2Cyt) + 3y(0)$

$$a_x = C(x^2 - y^2) + 2C^2 x t^2(x^2 - y^2) + 4C^2 x y^2 t^2$$

Example 2

We have:

$$\mathbf{V} = \overbrace{C t(x^2 - y^2)}^u \mathbf{i} - \overbrace{2Cxyt}^v \mathbf{j} + \overbrace{3y}^w \mathbf{k}$$

- The y-component:

$$a_y = \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z}$$

- Evaluating terms:

$$a_y = -2Cxy + Ct(x^2 - y^2)(-2Cyt) + (-2Cxyt)(-2Cxt) + 3y(0)$$

$$a_y = -2Cxy - 2C^2 yt^2(x^2 - y^2) + 4C^2 x^2 yt^2$$

Example 2

We have:

$$\mathbf{V} = \overbrace{C t(x^2 - y^2)}^u \mathbf{i} - \overbrace{2Cxyt}^v \mathbf{j} + \overbrace{3y}^w \mathbf{k}$$

- The z-component:
$$a_z = \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z}$$
- Evaluating terms: $a_z = 0 + Ct(x^2 - y^2)(0) + (-2Cxyt)3 + 3y(0)$, $a_z = -6Cxyt$
- Simplifying some of the terms, the acceleration vector is:

$$\begin{aligned} \mathbf{a} = \frac{d\mathbf{V}}{dt} = & \{C(x^2 - y^2) + 2C^2xt^2(x^2 - y^2) + 4C^2xy^2t^2\} \mathbf{i} \\ & + \{-2Cxy - 2C^2yt^2(x^2 - y^2) + 4C^2x^2yt^2\} \mathbf{j} - \{6Cxyt\} \mathbf{k} \end{aligned}$$

Example 2

We have:

$$\mathbf{a} = \frac{d\mathbf{V}}{dt} = \{C(x^2 - y^2) + 2C^2xt^2(x^2 - y^2) + 4C^2xy^2t^2\} \mathbf{i}$$

$$+ \{-2Cxy + -2C^2yt^2(x^2 - y^2) + 4C^2x^2yt^2\} \mathbf{j} - \{6Cxyt\} \mathbf{k}$$

(iii) Evaluating the acceleration vector \mathbf{a} at $(x, y, z, t) = (1, 1, 1, 1)$:

$$\mathbf{a} = \frac{d\mathbf{V}}{dt} = \{4C^2\} \mathbf{i} + \{-2C + 4C^2\} \mathbf{j} - \{6C\} \mathbf{k}$$

Ans.



Source: <http://mattybing1025.tumblr.com>

END NOTES

Presentation prepared and delivered by Dr. David Naylor.

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